

The presence of double T_g and phase separation in $Te_{80}Si_{20-x}Pb_x$ glasses

The occurrence of phase separation is of importance for preparation of materials with definite properties by controlled crystallization of glass [1–3]. In chalcogenides the phenomenon of phase separation has not been widely studied. Recently, the phase separation manifesting itself by double T_g has been found for Pb–Ge–As–Se glasses by calorimetric measurements and was confirmed by microscopic studies [4, 5]. The co-existence of two glassy phases has been also detected for $Te_{80}Ge_{12.5}Pb_{7.5}$ [6] and $Te_{77}Al_{23}$ [7] glasses. The possibility of phase separation in $Te_{80}Si_{20-x}Pb_x$ glasses has been shown by Lasocka [8]. The aim of this work was to confirm this prediction.

For preparation of alloys, high-purity elemental solids were used (5 N, 6 N). Weighed samples (20 g) were melted by induction for 3 min at about 1073 K, in evacuated quartz ampoules. A high-frequency generator was used. Small amounts of alloys thus prepared were remelted and then rapidly cooled by the gun technique [9] to produce a glass. Glassy samples of 10 mg were studied calorimetrically using a Perkin-Elmer DSC-2 unit.

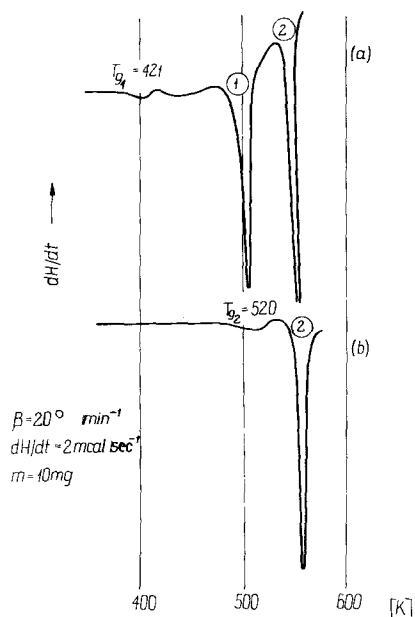


Figure 1 DSC traces taken for $Te_{80}Si_{17.5}Pb_{2.5}$ glass, as an example of double T_g occurrence: (a) first run, (b) second run, after previous heating to completion of the first exothermic transformation.

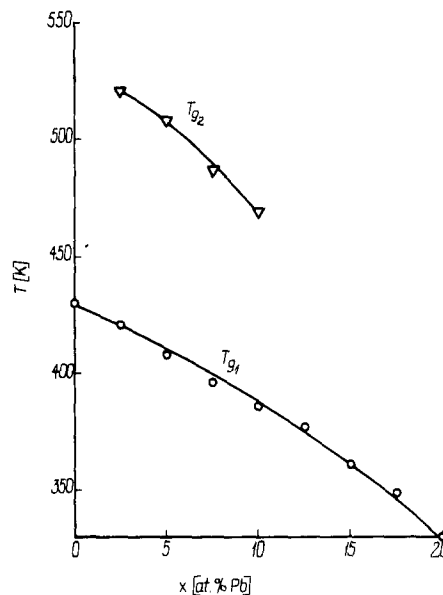


Figure 2 T_g of ternary glasses as a function of Pb concentration.

All glasses had the same thermal history. DSC curves taken for the first run exhibited only one glass transition temperature, T_{g1} (Fig. 1a). In order to read the second glass transition temperature, T_{g2} , the procedure proposed in [6] was used. Namely, samples were heated in a calorimeter at a rate of $20^\circ \text{ min}^{-1}$ to the temperature of the end of the first exothermic transformation, cooled at a rate of $320^\circ \text{ min}^{-1}$ and re-heated at a rate of $20^\circ \text{ min}^{-1}$. T_{g2} appeared within the temperature range of the previous peak of the first exothermic transformation.

We used a series of $Te_{80}Si_{20-x}Pb_x$ glasses (at%) with values of x changing every 2.5%. For each composition of glass, five replicate samples were studied and the mean values of T_{g1} and T_{g2} were calculated. The reproducibility of the results was better than 1° . Full experimental data are recorded in Table I and plotted in Figs. 1, 2 and 4.

Double T_g occurred for glasses containing 2.5 to 10 at% Pb. Depending on the composition, T_{g1} and T_{g2} were present within the temperature ranges 330 to 430 K and 469 to 520 K, respectively (Fig. 2). Glasses with lead concentration higher than 10 at% exhibited no double T_g .

The occurrence to two glass transition temperatures, T_{g1} and T_{g2} , points to the co-existence of two glassy phases in the as-quenched sample. The question arises which T_g corresponds to which

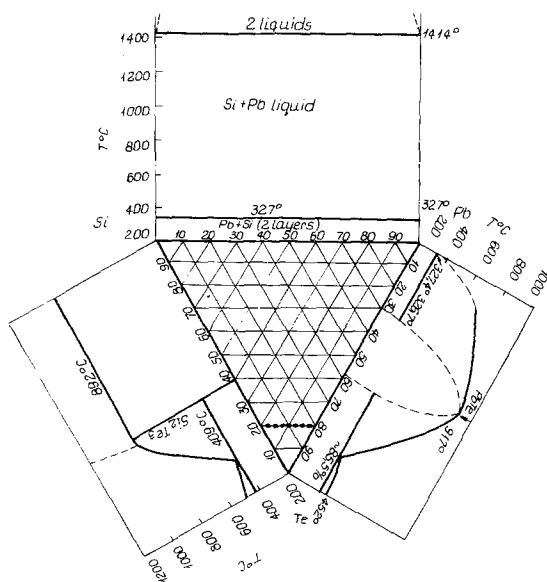


Figure 3 Compositions studied, shown in the concentration triangle of system Te-Si-Pb. Binary Te-Si, Te-Pb and Si-Pb diagrams were taken from refs. [10], [11], and [12], respectively.

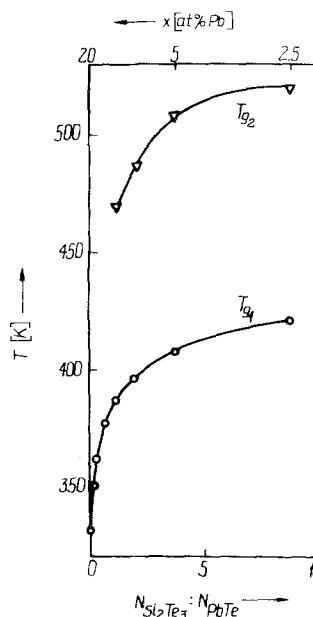


Figure 4 T_g as a function of molar ratio $Si_2Te_3 \cdot PbTe$.

phase. At equilibrium, the studied system Te-Si-Pb can be considered to be composed of Te, Si_2Te_3 and PbTe species (Fig. 3). In the glassy state, the existence of two super-saturated solid solutions PbTe(Te) and Si_2Te_3 (Te) may be assumed. Calorimetric results indicate that T_{g1} corresponds to the first exotherm, and T_{g2} to the second one. X-ray studies performed for two different samples heated to just above the first and second exotherms, respectively, indicate the occurrence of Te plus PbTe crystals in the first, and Si_2Te_3 in the second sample. The co-existence of two glassy phases, PbTe-rich and Si_2Te_3 -rich, also

seems to be confirmed by the nature of the changes in T_g plotted as a function of the molar concentration ratio $N_{Si_2Te_3} : N_{PbTe}$ (Fig. 4). The slope of the line within the range of low values of this ratio (high Pb concentrations) points to a strong dependence of T_{g1} on the Pb concentration. In the case of lower Pb concentrations (2.5 to 7.5 at%), even a great change in the ratio fails to affect T_{g1} to any great extent. The occurrence of T_{g2} within the range of high concentrations of Si_2Te_3 seems to be due to the existence of a Si_2Te_3 -rich glass.

TABLE I Glass transition temperatures, T_{g1} , T_{g2} , and molar fractions of Te, Si_2Te_3 , PbTe in $Te_{80}Si_{20-x}Pb_x$ glasses

	x (at%)								
	0	2.5	5	7.5	10	12.5	15	17.5	20
<i>Molar fraction</i>									
N_{Te}	0.5000	0.5125	0.5250	0.5375	0.5500	0.5625	0.5750	0.5875	0.6000
$N_{Si_2Te_3}$	0.5000	0.4375	0.3750	0.3125	0.2500	0.1875	0.1250	0.0625	0
N_{PbTe}	0	0.05	0.10	0.15	0.20	0.25	0.30	0.35	0.40
$N_{Si_2Te_3} :$	—	8.75	3.75	2.08	1.25	0.75	0.42	0.18	0
N_{PbTe}									
<i>Glass transition temperature (K)</i>									
T_{g1}	430	421	408	396	386	377	361	349	330
T_{g2}	—	520	508	487	469	—	—	—	—

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Preparation of copper-coated titania particles for composites

In recent years, various methods for production of metal ceramic particulate composites have been developed based on powder and liquid metallurgy techniques [1–5]. Frequently, non-wettability between oxide particles and metals results in segregation of metal and ceramic phases and poor interfacial bonding in metal–ceramic particulate composites [6–7]. To improve the wettability, the ceramic particles are frequently coated with metals. Various coating techniques have been developed [8] of which electroless deposition is the method most commonly used [9]. Deonath and Rohatgi [10] have used this procedure to coat copper on mica particles. The major steps involved in the electroless method are: (a) activation of the surface of the ceramic particles by deposition of a noble metal such as Pd, Pt and Ag; (b) deposition of metal on the activated surface from a reducing bath containing metal ions.

Owing to the large surface area of ceramic particles, uniform activation throughout the surfaces can be achieved only with a large amount of activator. As a result, the process frequently becomes uneconomical with conventional acti-

vators. In this communication, we report a new method for coating titania (TiO_2) particles with copper (thickness range 2 to 15 μm) employing a relatively inexpensive activator – copper tartrate (CuT). Experiments were also carried out to coat copper onto TiO_2 particles using conventional activator $\text{SnCl}_2/\text{PdCl}_2$ solution [6]. The results obtained from both techniques are compared.

TiO_2 powder of particle size 1 to 20 μm was supplied by M/s Travancore Titanium Products Ltd, Trivandrum. Copper tartrate (CuT) solution was prepared by mixing sodium potassium tartrate

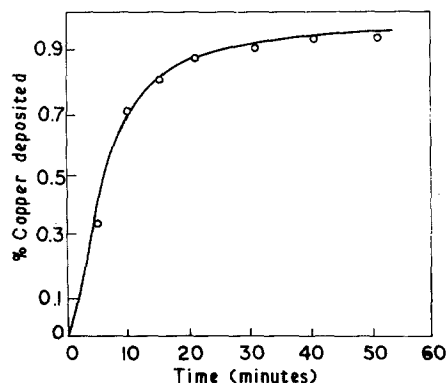


Figure 1 Copper tartrate adsorption on TiO_2 particles as a function of time.